

A New Tool For Analyzing Nonlinear Systems:

The Weighted Incremental Norm

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ILLUSTRATIVE EXAMPLES

Missile Control Problem

Highly Non Linear Model (Reichert)

$$\begin{aligned}\dot{\alpha} &= \cos(\alpha)K_{\alpha}MC_n(\alpha, \delta) + q \\ \dot{q} &= K_qM^2C_m(\alpha, \delta)\end{aligned}$$

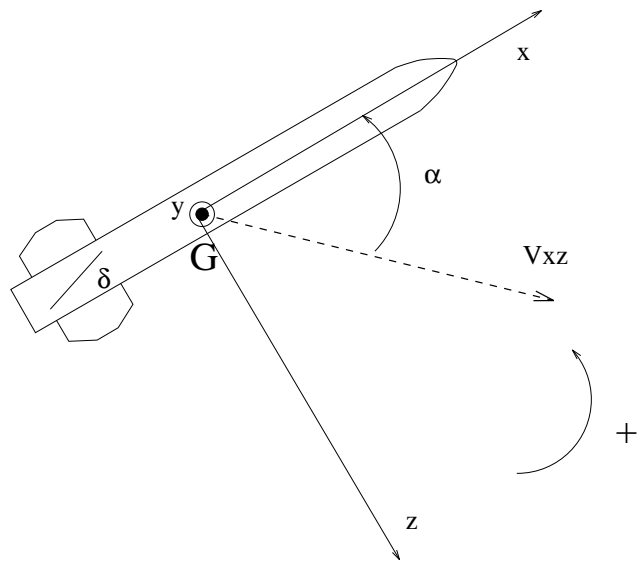
with Uncertain Stability Derivatives

$$C_n(\alpha, \delta) = a_n\alpha^3 + b_n|\alpha|\alpha + c_n\left(2 - \frac{M}{3}\right)\alpha + d_n\delta$$

$$C_m(\alpha, \delta) = a_m\alpha^3 + b_m|\alpha|\alpha + c_m\left(-7 + \frac{8M}{3}\right)\alpha + d_m\delta$$

Output: $\eta = \frac{K_z}{g_{grav}}M^2C_n(\alpha, \delta, M)$

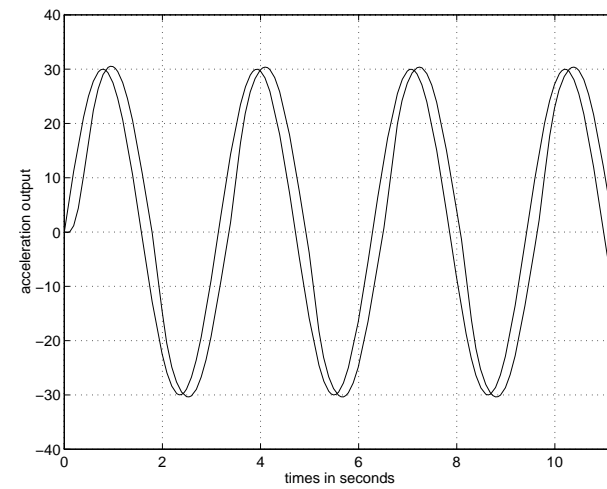
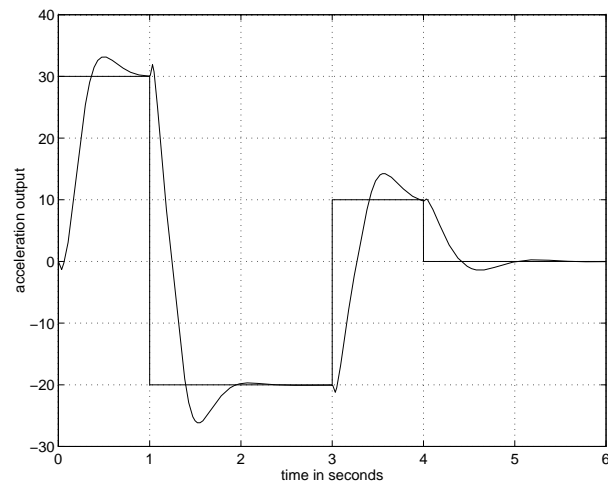
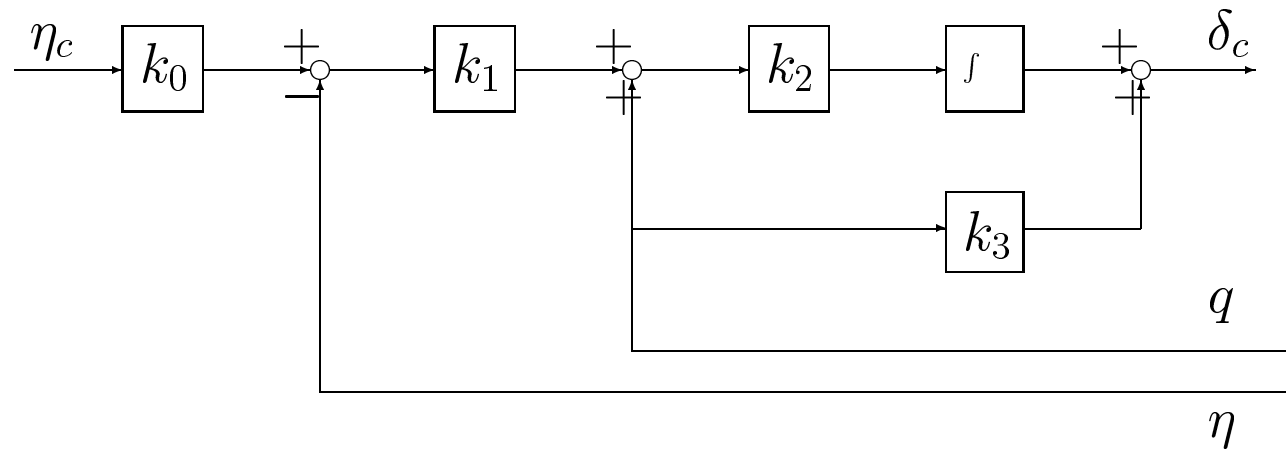
Actuator: $\delta(s) = \frac{\omega_a^2}{s^2 + 2\xi_a\omega_a s + \omega_a^2}\delta_c(s)$



Control objectives

- step tracking, time constant ≤ 0.35 s, low steady state error, overshoot $\leq 20\%$.
- sinusoid tracking

PI Controller: classical design



Nonlinear PI(D) controllers

Typical applications:

- Speed-up delayed systems
- Adaptation of the step tracking
- Nonlinear “filtering effects”

Methods

- Gain scheduling rules
- Fuzzy rules (fuzzy PID controllers).
- etc.

Control objectives

- step tracking, time constant, low steady state error, overshoot.
- rejection of perturbation, sinusoid tracking.

NECESSITY OF A THEORETICAL FRAMEWORK

Two problems

1. How to reduce performance/robustness to a mathematical criterium ?
2. How to test the corresponding conditions in an efficient way ?

INCREMENTAL NORM AS A POSSIBLE FRAMEWORK

From linear control to nonlinear H_∞ control

Main fact: In linear context the weighted H_∞ approach

\Rightarrow Is it possible to extend the weighted H_∞ approach to the nonlinear context?

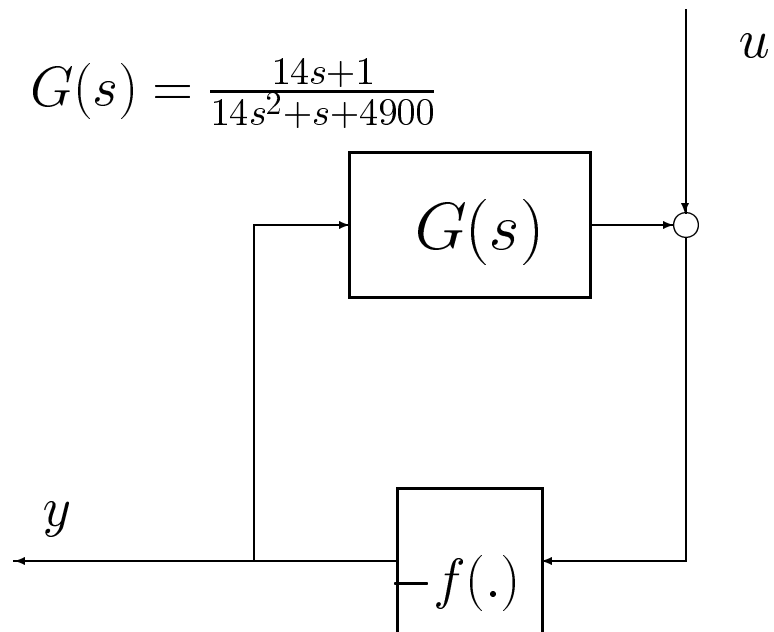
Two possible solutions

- 1– \mathcal{L}_2 gain.
- 2– Incremental gain (Lipschitz constant).

\Rightarrow Only the incremental framework allows to take into account performance requirements !

Limits of \mathcal{L}_2 gain stability

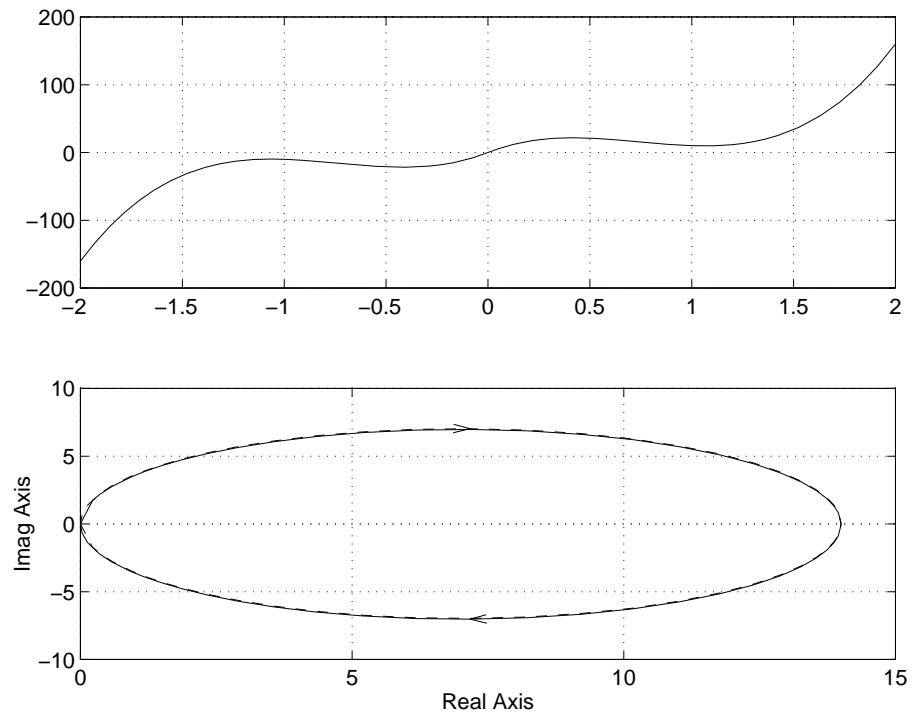
Considered system



$$G(s) = \frac{14s+1}{14s^2+s+4900}$$

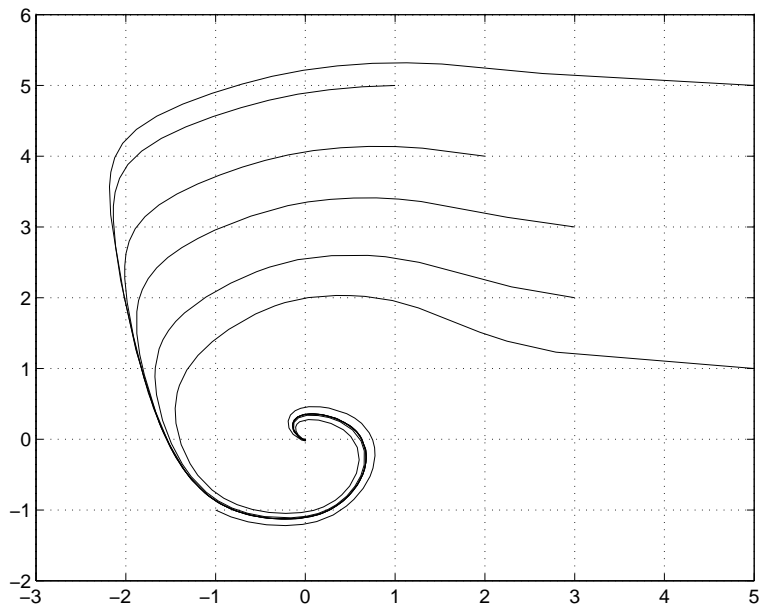
$$f(p) = 90p^3 - 200p|p| + 120p$$

Stability analysis via circle criterium

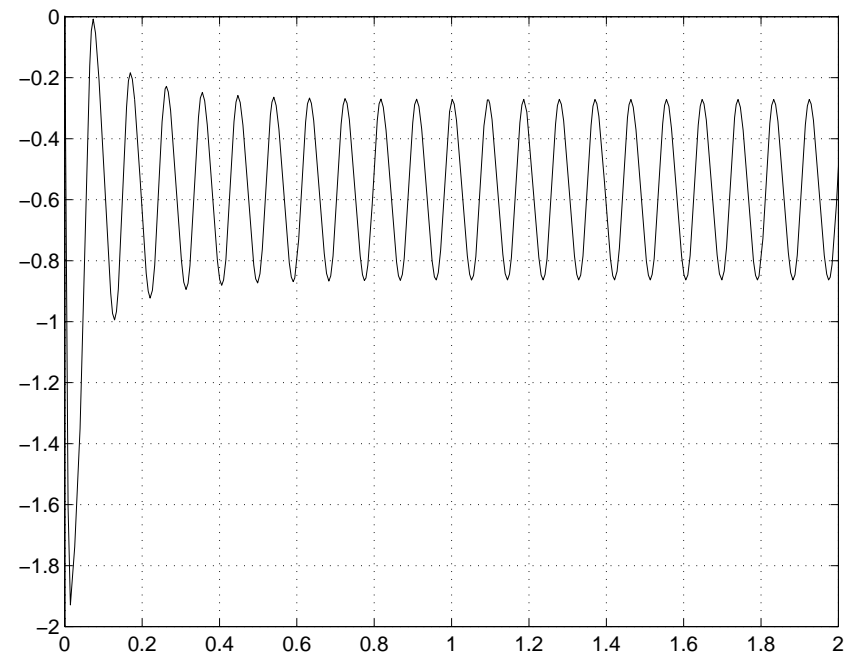


Limits of \mathcal{L}_2 gain stability (II)

Response to initial conditions



Step response



Incremental Norm: performance and robustness requirements

Incremental norm allows to take into account

Qualitative specifications

- Unique steady state properties
- Constant/periodic output asymptotically obtained from constant/periodic input
- Lyapunov stability of the unperturbed motions

Quantitative specifications

- Tracking error norm versus specific type of inputs
- Robustness with respect to uncertainties
- *Desensitivity* with respect to unmeasured perturbations and uncertainties

Considered systems

In the sequel, we consider systems with the differential representation

$$\Sigma \begin{cases} \dot{x}(t) = f(x(t), u(t)) \\ y(t) = h(x(t), u(t)) \\ x(t_0) = x_0 \end{cases} \quad (1)$$

where $x(t) \in \mathcal{R}^n$, $y(t) \in \mathcal{R}^m$, and $u(t) \in \mathcal{R}^p$.

f and h are C^2 , uniformly Lipschitz and such that $f(x_0, 0) = 0$ and $h(x_0, 0) = 0$.

Definition Σ is \mathcal{L}_2 gain stable if there exists $\gamma \geq 0$ such that for any $u \in \mathcal{L}_2$, one has $\|\Sigma(u)\|_2 \leq \gamma \|u\|_2$.

Definition Σ is incrementally stable on \mathcal{L}_2 if there exists $\eta \geq 0$ such that for any $u_1, u_2 \in \mathcal{L}_2$, one has $\|\Sigma(u_1) - \Sigma(u_2)\|_2 \leq \eta \|u_1 - u_2\|_2$.

CHARACTERIZATION OF INCREMENTAL STABILITY

Exactly testing incremental stability is a difficult problem

Let us characterize the incremental norm of this affine nonlinear system:

$$\begin{cases} \dot{x}(t) = f(x(t)) + g(x(t))u(t) \\ y(t) = h(x(t)) \\ x(t_0) = x_0 \end{cases} \quad (2)$$

Theorem Let η a positive constant. The dynamical system (2) has a incremental gain less or equal to η if there exists a C^1 function, S defined from $\mathcal{R}^n \times \mathcal{R}^n$ into \mathcal{R} , which satisfies for all $x_1, x_2 \in \mathcal{R}^n$ the following conditions:

$$S(x_0, x_0) = 0$$

$$S(x_1, x_2) \geq 0$$

$$\begin{aligned} \frac{\partial S}{\partial x_1}(x_1, x_2)f(x_1) + \frac{\partial S}{\partial x_2}(x_1, x_2)f(x_2) + \frac{1}{4}\eta^{-2}\frac{\partial S}{\partial x_1}(x_1, x_2)g(x_1)g^T(x_1)\frac{\partial S}{\partial x_1}(x_1, x_2) + \\ (h(x_1) - h(x_2))^T(h(x_1) - h(x_2)) \leq 0 \end{aligned}$$

$$\frac{\partial S}{\partial x_1}(x_1, x_2)g(x_1) + \frac{\partial S}{\partial x_2}(x_1, x_2)g(x_2) = 0$$

HOW TO TEST THE CORRESPONDING CONDITIONS IN AN
EFFICIENT WAY ?

Quadratic incremental stability

⇒ Quadratic type solutions allows to obtain a good compromise between complexity and conservatism.

More generally, system (1) is said to be *quadratically incrementally stable* if there exist $P = P^T > 0$, $\epsilon > 0$, $\sigma_{f_u} > 0$ such that for any $x \in \mathcal{R}^n$ and $u \in \mathcal{R}^p$, one has

$$(i) \quad P \frac{\partial f}{\partial x}(x, u) + \frac{\partial f}{\partial x}^T(x, u) P \leq -\epsilon I_n$$

$$(ii) \quad \left(\frac{\partial f}{\partial u}\right)^T \left(\frac{\partial f}{\partial u}\right) \leq \sigma_{f_u} I$$

which implies that there exists η_x such that for any $u_1, u_2 \in \mathcal{L}_2$, one has

$$\|x_1 - x_2\|_2 \leq \eta_x \|u_1 - u_2\|_2.$$

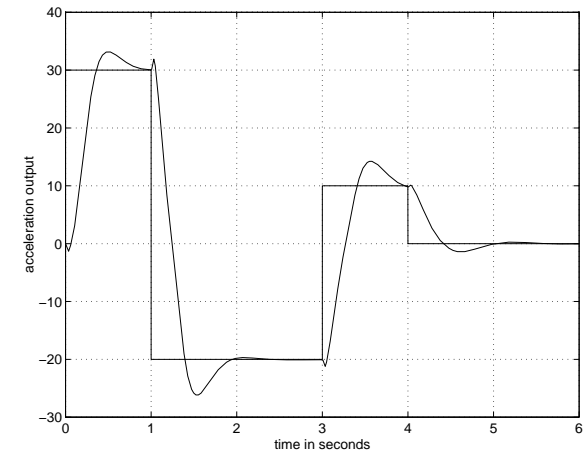
Stronger notion but ...

(i) can be ensured by *Convex Optimization* over LMI constraints

QUALITATIVE PROPERTIES OF QUADRATICALLY
INCREMENTALLY STABLE SYSTEMS

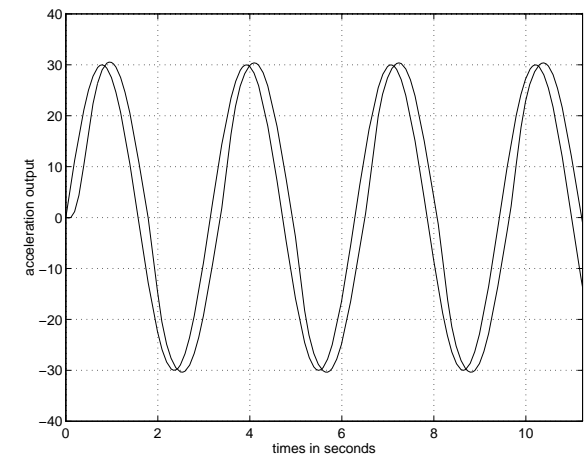
For a constant input...

$$x(t) \rightarrow \text{constant}$$



For T periodic input...

$$x(t) \rightarrow T \text{ periodic output}$$



+ Many properties with respect to initial condition and perturbations.

Testing incremental stability: LMI approaches

Condition to verify:

$$(i) \quad P \frac{\partial f}{\partial x}(t, x, u) + \frac{\partial f}{\partial x}^T(t, x, u) P \leq -\epsilon I_n$$

Interpretation: quadratic stability of:

$$\dot{\delta x} = \frac{\partial f}{\partial x}(t, x, u) \delta x$$

Two possible modeling:

1. Polytopic model

$$\left\{ \frac{\partial f}{\partial x}(t, x, u) \right\} \subset \left\{ F(\theta(t)) = \sum_{i=1}^r \lambda_i(t) A_i, \begin{cases} \sum_{i=1}^r \lambda_i(t) = 1 \\ \lambda_i(t) \geq 0 \end{cases} \right\}$$

2. so-called “Linear Fractional Transformation” model

$$\left\{ \frac{\partial f}{\partial x}(t, x, u) \right\} \subset \{ F(\theta(t)) = A + B_p \Delta(\theta(t)) (I - D_{qp} \Delta(\theta(t))) C_q \}$$

with

$$\Delta(\theta(t)) = \mathbf{diag}(\theta_1(t) I_{n_1}, \dots, \theta_r(t) I_{n_r}), \quad \theta_i(t) \in [a_i, b_i]$$

ILLUSTRATIVE EXAMPLES

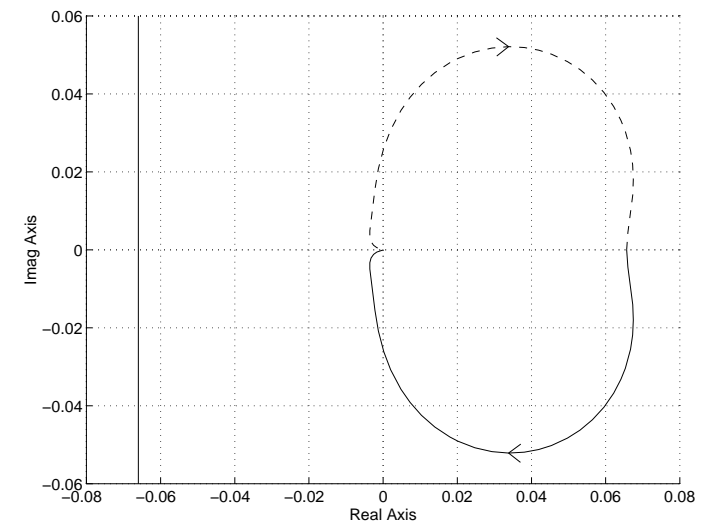
PI controlled missile incremental stability: circle criterion

$h(s) = c_q(sI - A)^{-1}b_p$ connected with $k(t)$

$$A = \begin{bmatrix} K_\alpha M c_n (2 - \frac{M}{3}) & 1 & K_\alpha M d_n & 0 & 0 \\ K_q M^2 c_m (-7 + 8\frac{M}{3}) & 0 & K_q M^2 d_m & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ -k_1 k_2 \frac{K_z}{g} M^2 c_n (2 - \frac{M}{3}) & k_2 & -k_1 k_2 \frac{K_z}{g} M^2 d_n & 0 & 0 \\ 0 & k_3 w_a^2 & -w_a^2 & -2\xi_a w_a & w_a^2 \end{bmatrix}$$

$$b_p = \begin{bmatrix} K_\alpha M \\ 2K_q M^2 \\ 0 \\ 0 \end{bmatrix} \quad c_q = [1 \ 0 \ 0 \ 0 \ 0] \quad k(t) \in [-15, 0]$$

Nyquist plot of $h(s)$
(Circle Criterion)



PI controlled missile incremental stability: an LMI approach

- Polytopic modeling

$$\frac{\partial f}{\partial x}(t, x, u) = A + k(t)bc = \lambda(t)A + (1 - \lambda(t))(A - 15bc)$$

- Associated optimization problem: $P > 0$

$$A^T P + P A < 0 \text{ and } (A - 15bc)^T P + P(A - 15bc) < 0$$

- Readily solved by **LMITOOL** :

$$P = \begin{bmatrix} 6.5479 & 0.0974 & -0.0927 & -0.0009 & -0.6899 \\ 0.0974 & 0.2843 & -0.3851 & -0.0033 & 0.6318 \\ -0.0927 & -0.3851 & 0.7955 & 0.0056 & -0.7863 \\ -0.0009 & -0.0033 & 0.0056 & 0.0001 & -0.0069 \\ -0.6899 & 0.6318 & -0.7863 & -0.0069 & 2.3722 \end{bmatrix}$$

Nonlinear PI(D) controller incremental stability: circle criterion

At the end of the talk !

GUARANTEEING DESIGN SPECIFICATIONS: QUANTITATIVE
ASPECTS

Quantitative analysis: from nominal performance...

Nominal performance = tracking of input signals in R_d^e for a nonlinear system

R_d^e defined by W_1 such that

$$\|P_T W_1^{-1}(r)\|_2 \ll \|P_T r\|_2 \quad \forall r \in R_d^e$$

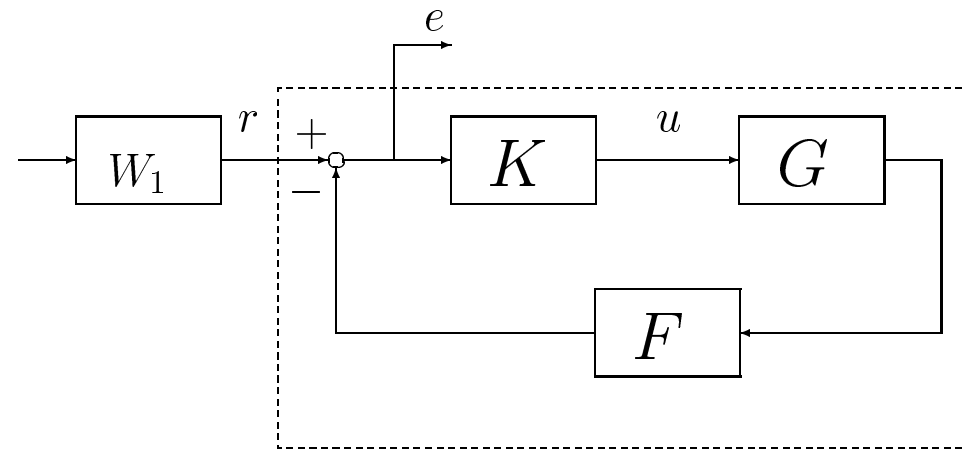
Tracking if $\exists T_0 \geq 0, \forall T \geq T_0 :$

$$\|P_T e\|_2 \ll \|P_T r\|_2 \quad \forall r \in R_d^e$$

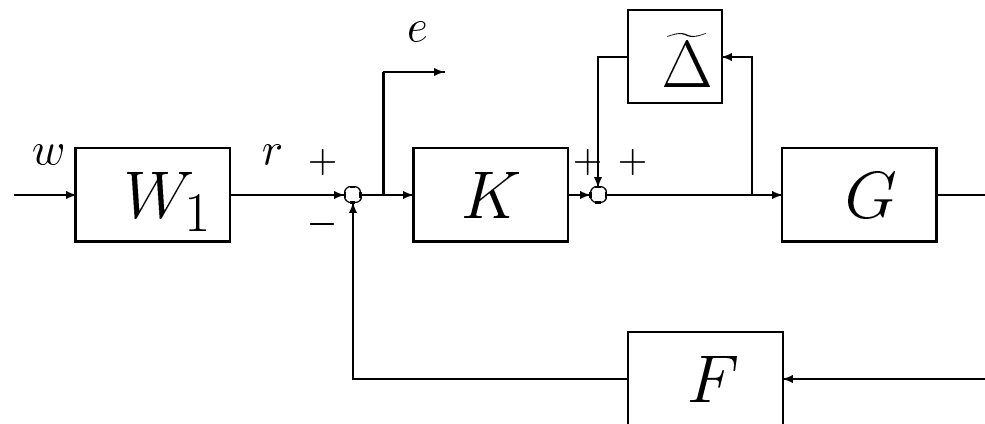
The signal in R_d^e are tracked if

$$\|(I + FGK)^{-1}W_1\|_{\Delta} \leq 1$$

In the linear case, H_{∞} performance is recovered.



Quantitative analysis: ...to robust performance



In the extension of H_∞ framework:

- Robust incremental stability analysis
- Robust incremental performance analysis

HOW TO (PRACTICALLY) CHECK THE PREVIOUS
CONDITIONS?

Scaling and small gain type condition

Theorem The previous interconnected system is incrementally stable, for any Δ whose incremental norm is less than 1, if there exists a scaling $D(s)$ satisfying:

$$\text{for all } \omega, \quad M_{qp}(j\omega)^* D(j\omega) M_{qp}(j\omega) - D(j\omega) < 0$$

with

$$D(\Delta) \triangleq \mathbf{diag}(d_1 I, \dots, d_i I, \dots, d_r I)$$

where the scalars $d_i = \lambda_i^2$ possibly depend on the frequency, if Δ_i is LTI

Multipliers and passive type condition

Theorem The previous interconnected system is incrementally stable, for any Δ which is incrementally passive, if there exists a multiplier $M_{mul} \in \mathcal{M}_{mul}(\Delta)$ satisfying:

$$\text{for all } \omega, \quad M_{mul}(j\omega)M_{qp}(j\omega) + (M_{mul}(j\omega)M_{qp}(j\omega))^* < 0.$$

where

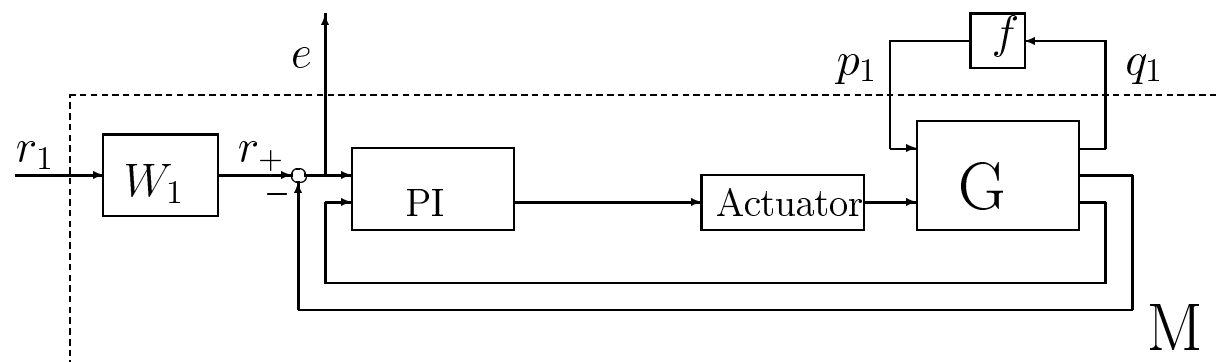
$$M_{mul} \triangleq \mathbf{diag}(m_1 I, \dots, m_i I, \dots, m_r I)$$

where m_i is possibly frequency dependent if Δ_i is LTI.

ILLUSTRATIVE EXAMPLES

PI controlled missile: nominal performance

Proved for $W_1(s) = 0.05 \frac{s+2.5}{s+0.25}$ by convex optimization

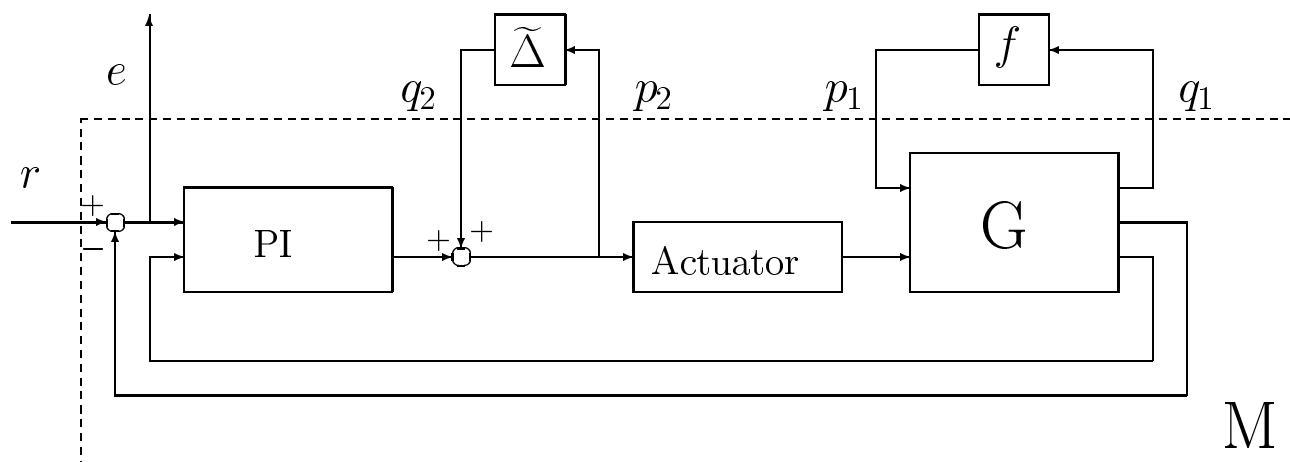


$$M \sim \begin{bmatrix} A_M & B_M \\ C_M & D_M \end{bmatrix}$$

Find $P, \beta > 0$ and $\lambda > 0$ such that:

$$\begin{bmatrix} A_M & B_M \\ C_M & D_M \\ 1 & 0 \\ 0 & I \end{bmatrix}^T \left[\begin{array}{ccc|ccc} 0 & 0 & 0 & P & 0 & 0 \\ 0 & 0 & 0 & 0 & -15\lambda & 0 \\ 0 & 0 & \beta & 0 & 0 & 0 \\ \hline P & 0 & 0 & 0 & 0 & 0 \\ 0 & -15\lambda & 0 & 0 & -2\lambda & 0 \\ 0 & 0 & 0 & 0 & 0 & -\beta I \end{array} \right] \begin{bmatrix} A_M & B_M \\ C_M & D_M \\ 1 & 0 \\ 0 & I \end{bmatrix} < 0$$

PI controlled missile: Robust performance



Performance : $W_1(s) = 0.05 \frac{s+2.5}{s+0.25}$

Robustness : 6dB input margin

Find $D(s) \triangleq \mathbf{diag}(d_1, d_2(s), d_3)$ such that

$$M(j\omega)^* D(j\omega) M(j\omega) - D(j\omega) < 0$$

Nonlinear PI Controller: an example